

# **Quantification of induced stiction in a MEMS**

**R. Ranganathan, T. Yu, N. Yadav, N. Johnson,  
A. Mellinger, R. Gale, and T. Dallas**

***Department of Electrical and Computer Engineering,  
Texas Tech University***



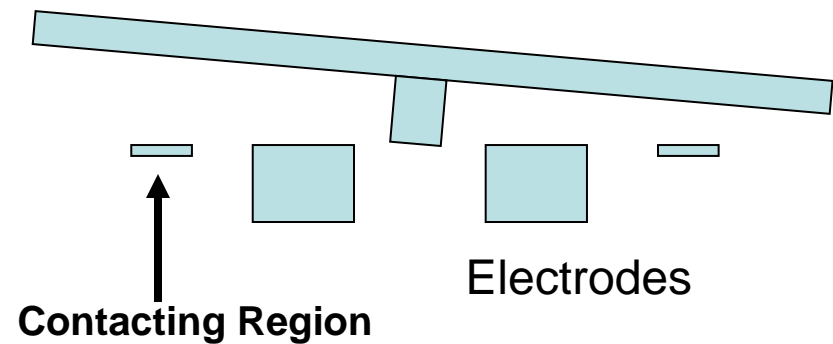
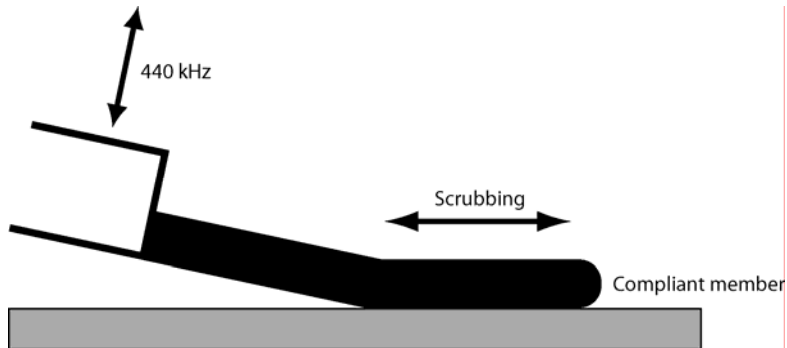
# Objective

**Improve fundamental understanding of stiction in MEMS devices allowing decreased packaging complexity and cost reduction.**

- **Use MOEMS as a test bed for stiction and friction characterization studies**
  - **Develop a model for the quantification of induced stiction under controlled operating conditions**
  - **Study the effect of stiction under elevated operating temperatures**

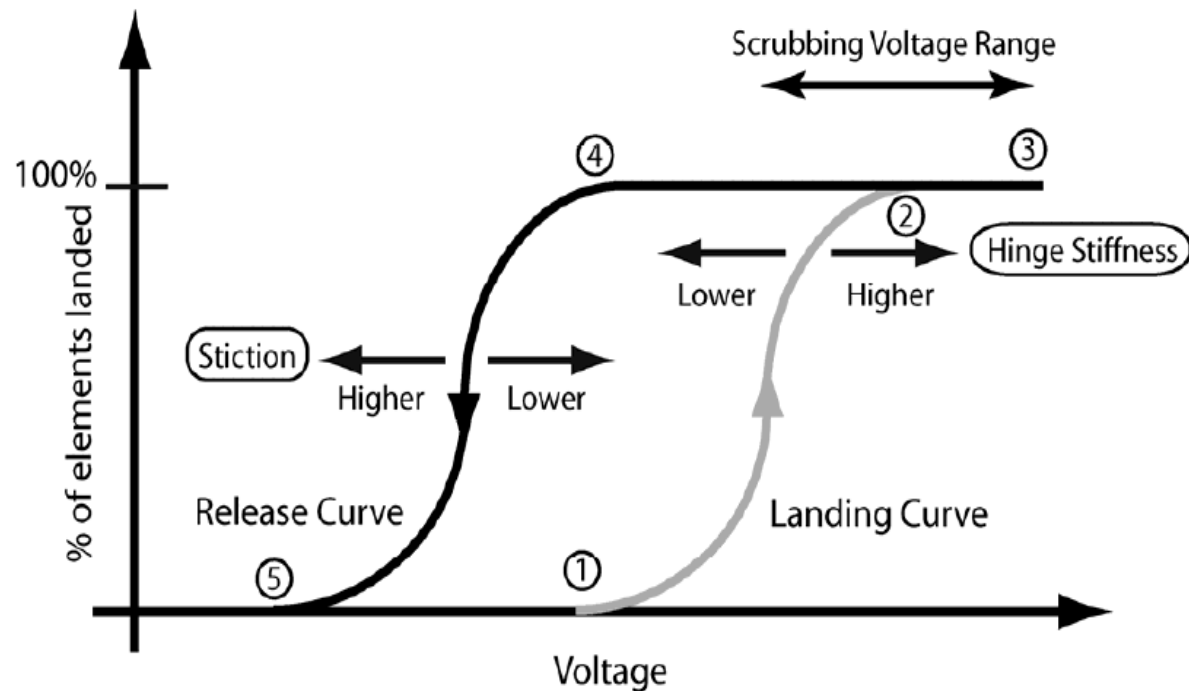


# Background

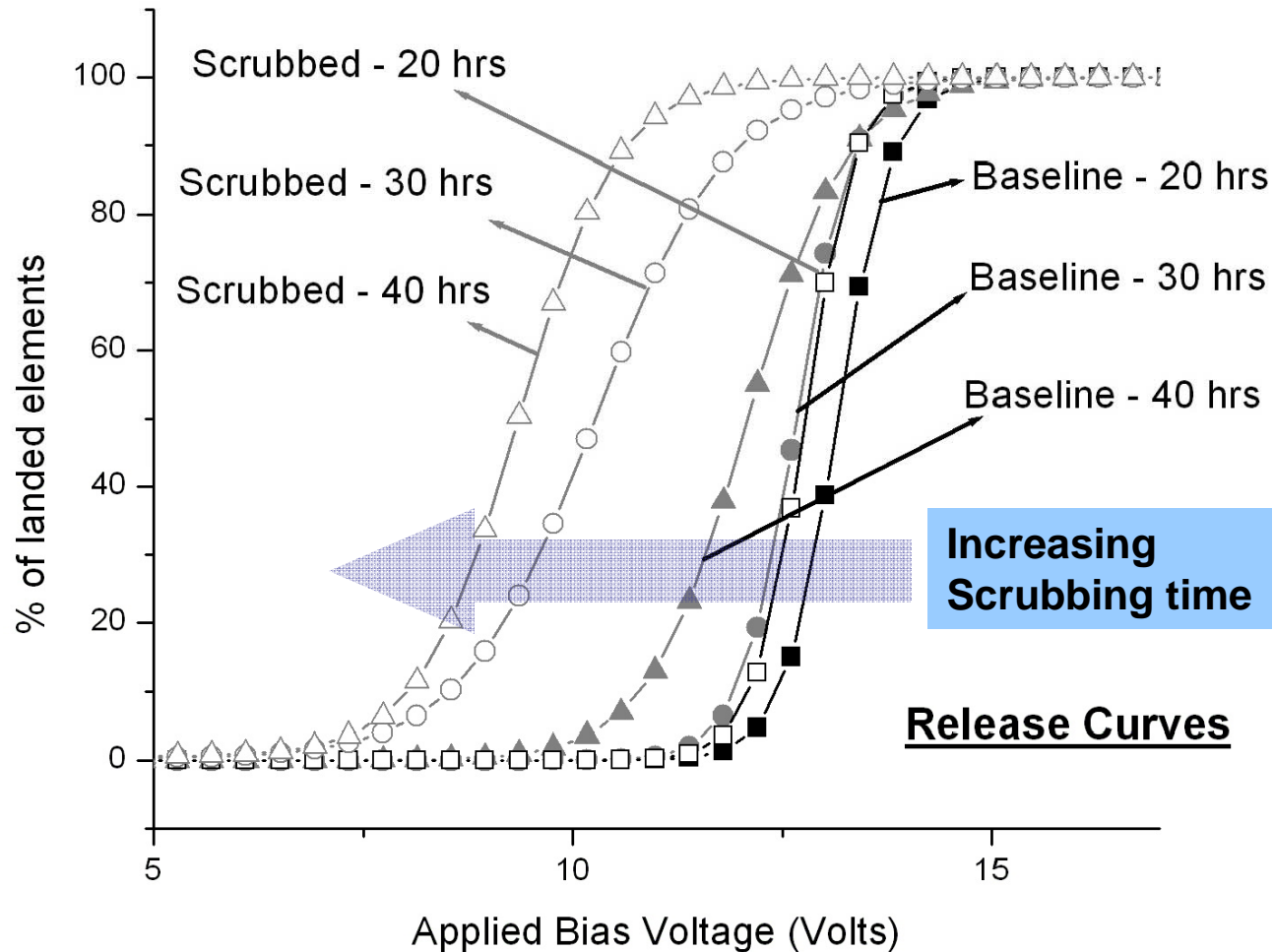


**Scrubbing** – Accelerated aging procedure by which a high frequency waveform is impressed on top of the standard DC bias applied to the micromirrors

Scrubbing initiates back and forth motion increasing Stiction inducing interactions.



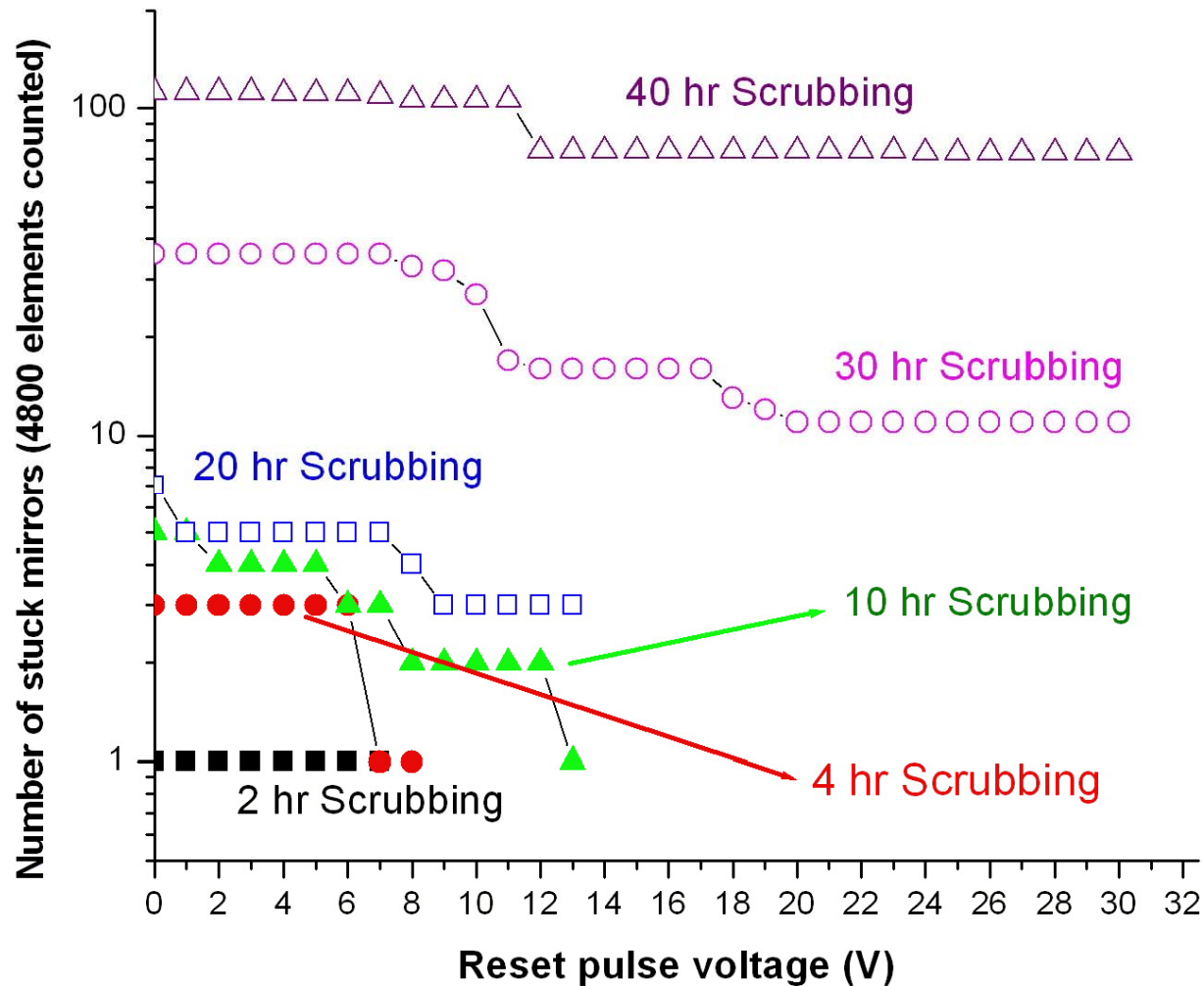
# Typical Results



**Scrubbing successful in promoting stiction with longer scrubbing time increasing Surface stiction**



# Typical results.... cont'd



**Bias Adhesion mapping – Application of progressively increasing magnitude reset pulses to release stuck mirrors**

**Release Voltage and Reset pulse voltage values – Good Stiction indicators**



# Device modeling – Capacitance based modeling

Equation of motion

$$I \frac{d^2 \theta}{dt^2} + \eta \frac{d\theta}{dt} + k_\theta \theta = M_e$$

Energy of the system

$$W = \frac{1}{2} CV^2$$

System Capacitance

$$C = \frac{\epsilon_o w}{\theta} \ln \left[ \frac{1 - \left( \frac{x_1}{g} \right) \tan \theta}{1 - \left( \frac{x_1 + L}{g} \right) \tan \theta} \right]$$

Un-actuated mirror

Mirror tilted to one side

Energy of the system

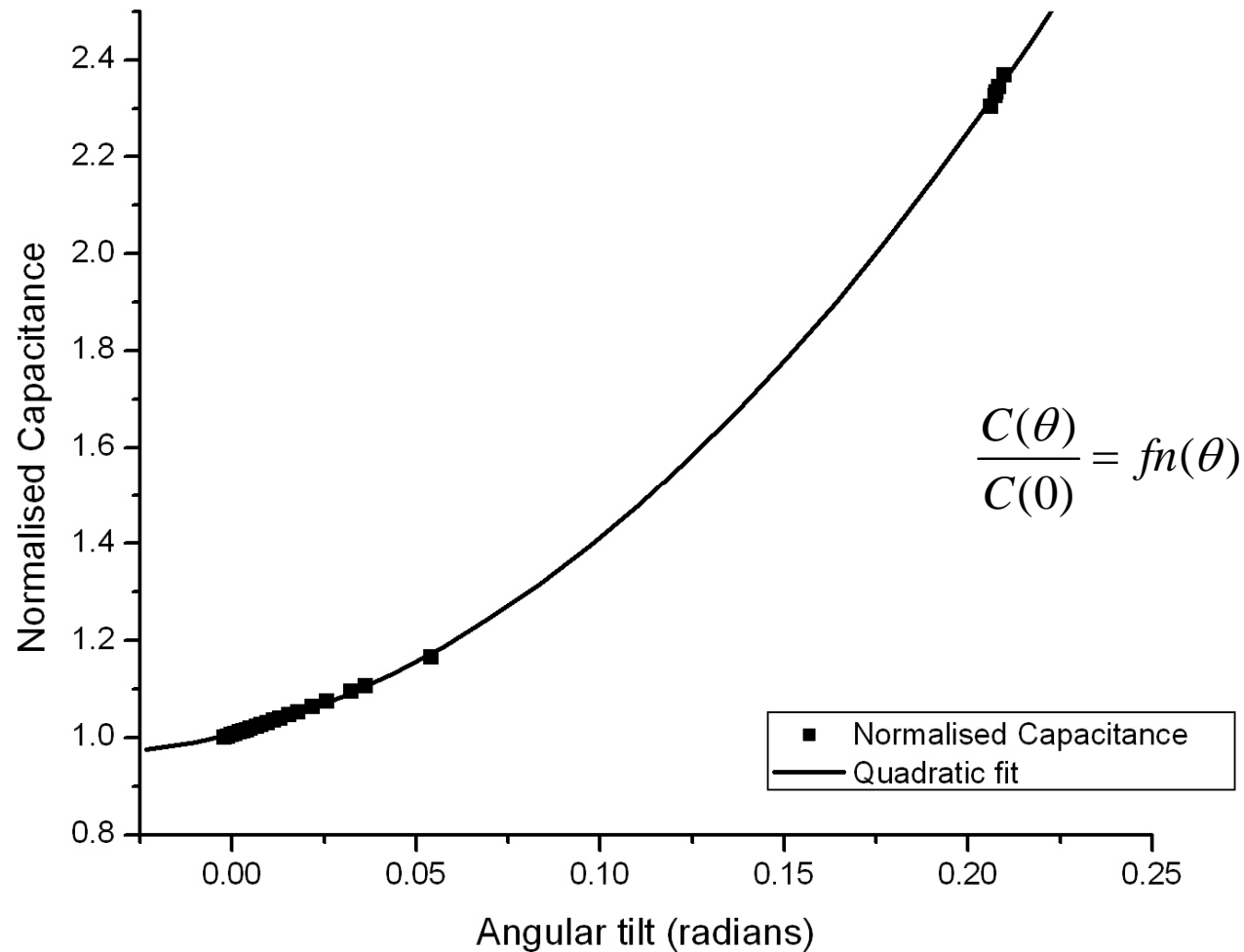
$$W = \frac{1}{2} V^2 C(0) [fn(\theta)]$$

$$\frac{C(\theta)}{C(0)} = fn(\theta)$$

Electrostatic torque is given by the negative gradient of the energy with respect to the angular tilt.



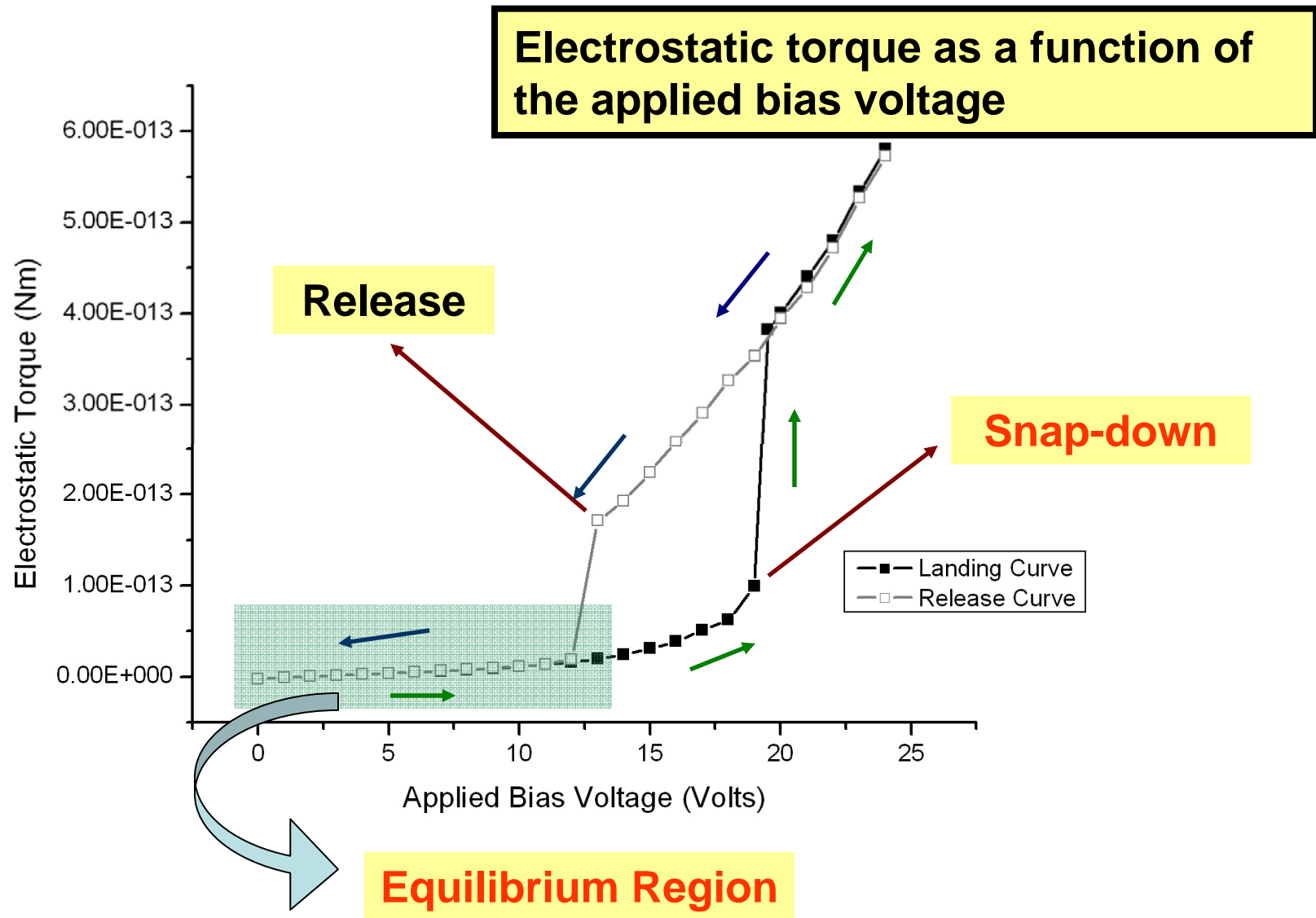
# Modeling



**Normalized Capacitance of the landing side electrode**

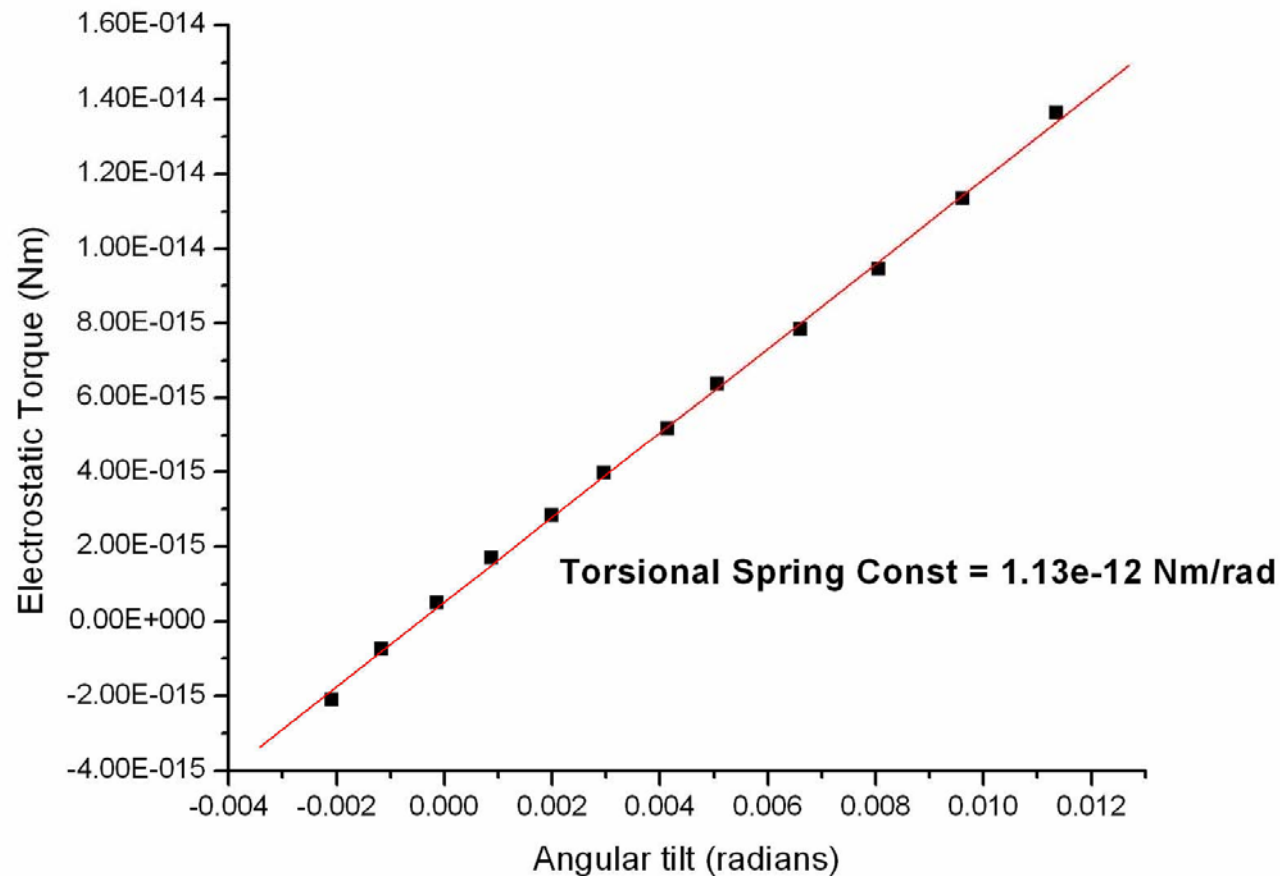


# Modeling





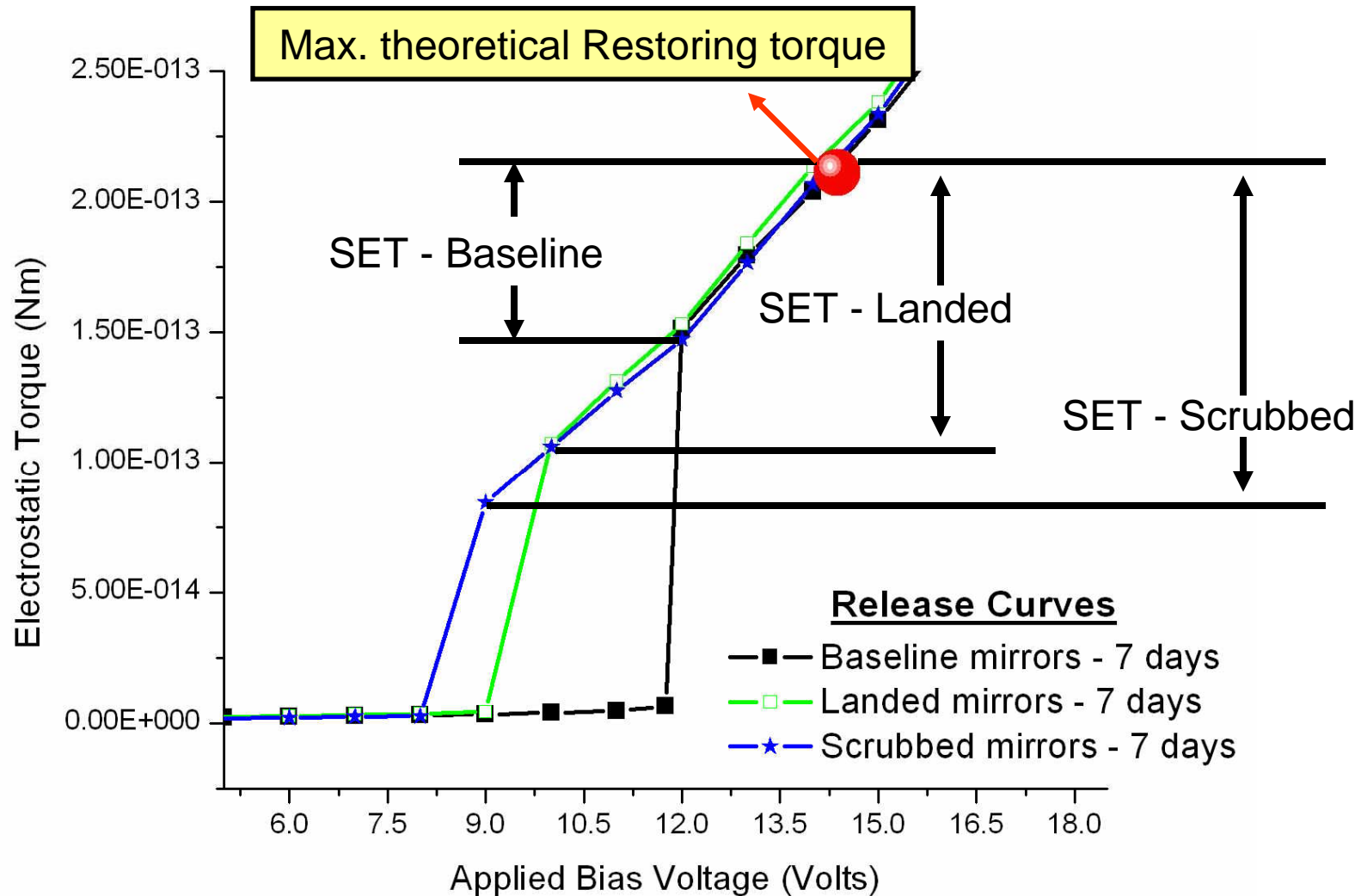
# Calculation of Torsional Spring Constant



**Maximum Restoring Torque = Spring Constant \* Maximum angular deflection**



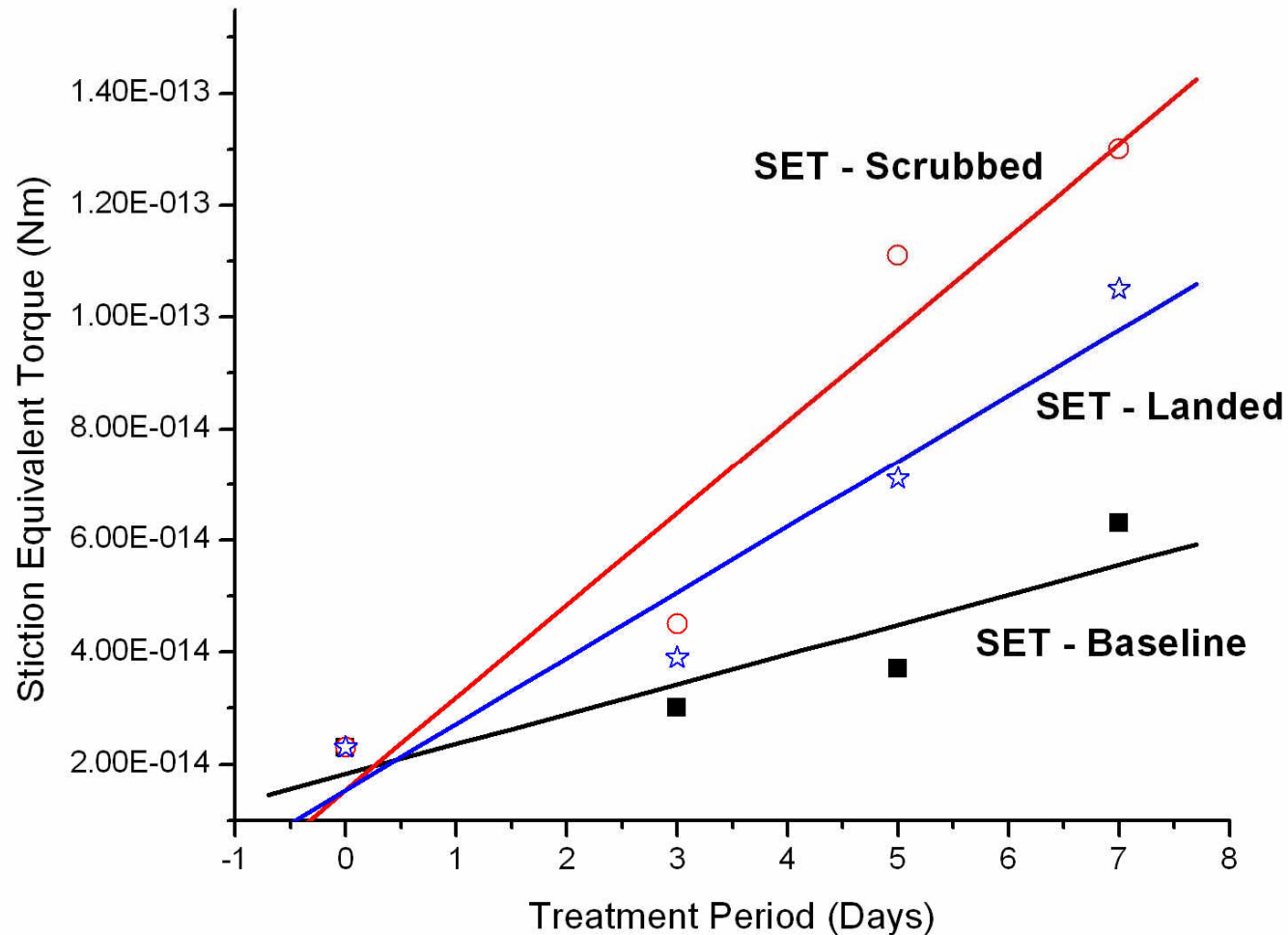
# Calculation of *Stiction-equivalent* torque (SET)



**Stiction Equivalent torque translates Release Voltages into easily comparable torque values**



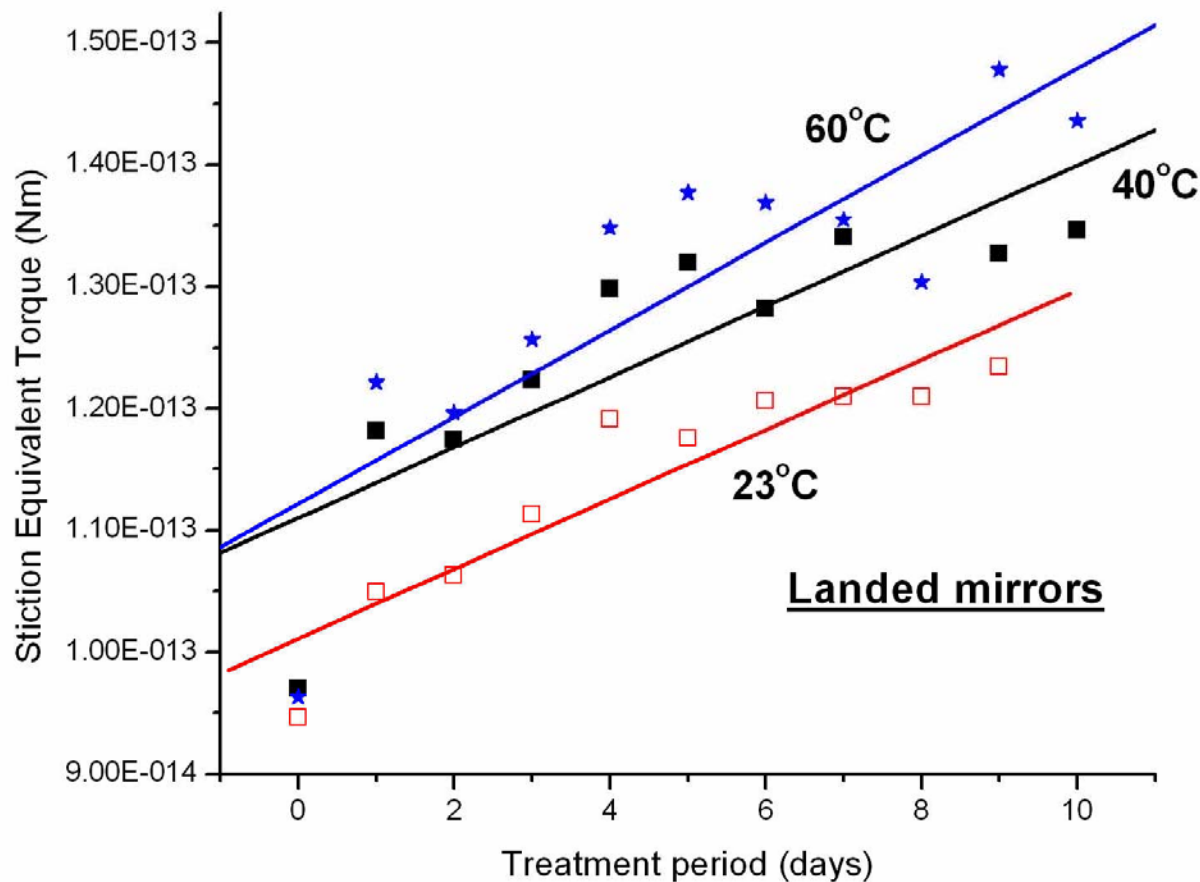
# Stiction equivalent torque (SET)



**Increase in the stiction equivalent torque is highest in the case of the Scrubbed device for the treatment period**



# Stiction characterization under elevated temperature operation

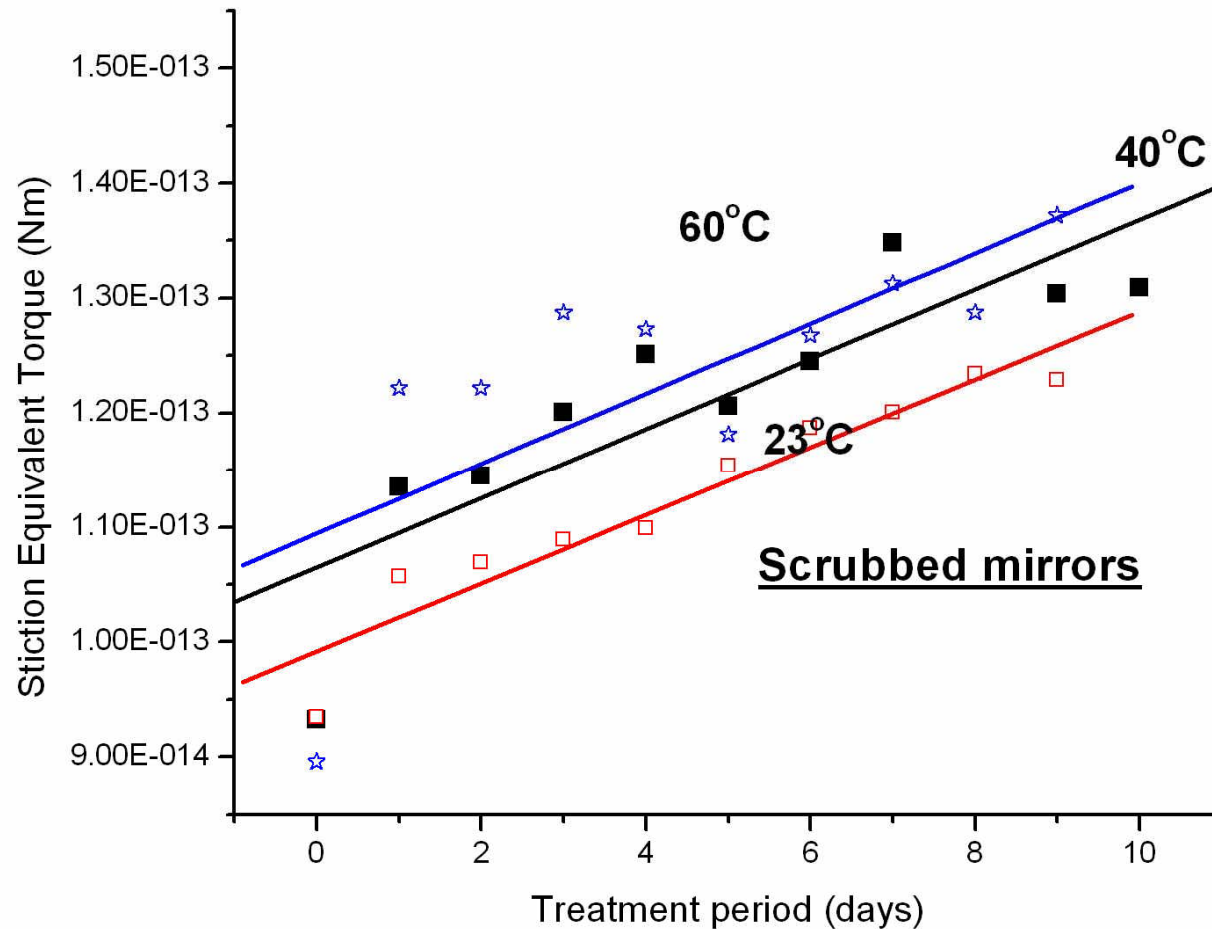


De-lidded mirrors subjected to Scrubbing and uneven duty cycle operation at 23°C, 40°C and 60°C for a period of 10 days.

Increase in Stiction observed with increase in operating temperature



# Stiction characterization under elevated temperature operation



Change in the Stiction Equivalent torque with period of treatment is similar for the Scrubbed and Landed devices



# Conclusions

- Established a reasonable model for translating Stiction indicators in terms of forces which can be easily compared
- Extended the analysis of Scrubbing technique for device operation under different temperatures
- Stiction is found to increase with increase in the operating temperature

## Future work

- Model the effects of Temperature and Humidity combined and individual contribution on the Stiction accrual
- Model SET calculation for Reset Voltage application procedure
- Analysis of device operation under different lubricant environments to aid in better packaging techniques

## Acknowledgements

National Science Foundation ECS #0326218 and the Maddox Endowment at TTU



NANO TECH CENTER

TEXMEMS VII